

THERMAL CONDUCTIVITY OF HEAVY WATER AT HIGH PRESSURES  
AND ITS DEPENDENCE ON DENSITY

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We employed the plane horizontal layer method to derive data on the coefficient of thermal conductivity for heavy water, and these data are compared with values for ordinary water.

Heavy water ( $D_2O$ ) is used extensively in numerous heat and power generating installations, including nuclear plants. Experimental research into the thermal conductivity of  $D_2O$  has been carried out in many countries, and a rather large quantity of papers is presently in publication [1-14], with brief reviews of these publications presented in [15-17]. An analysis of all experimental studies published prior to 1976 can be found in [16] which also provides suggested handbook data on the coefficient of thermal conductivity for  $D_2O$  below 250 MPa.

It is the goal of this paper to expand the range of the experimental research dealing with pressure, as well as to refine existing data on the thermal conductivity of  $D_2O$ .

We chose the plane horizontal layer method to investigate the thermal conductivity of  $D_2O$ . The device that we used has been described in [18]. Its main parts are fabricated out of copper. The wires of the furnaces and thermocouples are insulated with glass filaments on a special winding stand and placed inside sheaths and small tubes made out of high-strength steel. Some of the components of the installation and the autoclave were chrome coated. Prior to being filled, the system was heated to 120-140°C and simultaneously evacuated. The  $D_2O$  used in the experiment was first cleansed of gases, producing a content of 99.75%.

The experimental error was  $\pm 1.6\%$ , the mean-square error was  $5.17 \text{ mW}/(\text{m}\cdot\text{K})$  or  $\pm 0.75\%$ , and the arithmetic mean of  $2.3 \text{ mW}/(\text{m}\cdot\text{K})$  or  $\pm 0.38\%$  was used to estimate the mean square error. Provision was made for the monitored losses of the installation in calculating the coefficient of thermal conductivity.

The experimental values for the coefficient of the thermal conductivity of the  $D_2O$  were obtained at temperatures of 20-200°C and at pressures of 0.1-400 MPa. The studies were conducted along isotherms at pressure intervals of 20 MPa. The minimum temperature drop across the  $D_2O$  layer amounted to 1.205°C. The thermostat temperature fluctuations amounted to 0.02 °C. Each point was checked 4-8 times, with the arithmetic mean value taken as the basis. The experiment was performed in such a manner that no deviation from the specified temperature values exceeded 0.3°C. For identical parameters the experimental points deviated from the arithmetic mean by no more than 0.75%.

Since the thermocouples of the heater and the "refrigerator" are in contact with the metal, in addition to the "refrigerator" thermocouples we used yet another thermocouple which was not in contact with the metal of the "refrigerator." This approach was first suggested and well described in [19].

The pressure was measured by means of an MP-2500 piston manometer, as well as with an SV26R superhigh-pressure-type manometer whose upper measurement limit was 5000 kgf/cm<sup>2</sup>, with an error of 1%. To attain the given pressure values in MPa, appropriate weight rings were added to the weights of the piston manometer.

The data obtained in this paper were compared with the results of [5-10, 13, 14] and with the recommended handbook data from [16]. These comparisons showed that the experimental data [5-7, 14] deviate by less than 1.6%, the handbook data [16] by 1.3% at pressures of

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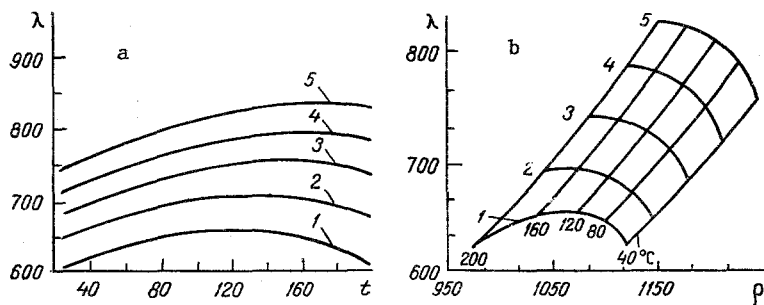


Fig. 1. The thermal conductivity of  $D_2O$  as a function of temperature (a) and density (b) at various pressures: 1)  $P = 20$  MPa; 2) 100; 3) 200; 4) 300; 5) 400.  $\lambda$ ,  $mW/(m \cdot K)$ ;  $t$ ,  $^{\circ}C$ ;  $\rho$ ,  $kg/m^3$ .

0.1-250 MPa, and the results of [8-10, 13] agree within limits of 1.6% with the exception of individual sections of certain of the references: for example, the data of [8, 9] are higher by 2-2.5% at pressures of 200-245 MPa and temperatures of 180-200 $^{\circ}C$ , while the data of [13] are lower by 2-3% at temperatures of 120-200 $^{\circ}C$  and at pressures of 100-150 MPa.

Analysis of the measurement results showed that the isobars of the  $D_2O$  thermal conductivity (Fig. 1a) exhibit a maximum that shifts as the pressure increases toward the higher temperatures. The shift in the maximum for the  $D_2O$  is smaller than in the case of ordinary water ( $H_2O$ ); at the 400 MPa isobar the  $D_2O$  maximum is found at a temperature close to 170 $^{\circ}C$ , while for  $H_2O$  this displacement is noted as early as the 200 MPa isobar [18]. Similar displacements had been noted earlier in [17, 20, 21].

The  $D_2O$  coefficient of thermal conductivity is smaller than the  $H_2O$  thermal conductivity. This is apparently associated with the fact that the mass of the  $D_2O$  particle is greater than the mass of the  $H_2O$  particle, i.e., it exhibits greater inertia, and inertia reduces the intensity of the thermal motion and, consequently, the thermal conductivity. Such an explanation is in agreement with [22, 23].

Water is an associated liquid, and if these associates are treated as new "molecules" which participate in the transport of heat, the larger the associates, the more substantial the coefficient of thermal conductivity. Eigen in [24] examines the process of energy transfer in association (the energy of breaking and restoring hydrogen bonds) through the structural diffusion of these associates, which serves to explain the high values for the coefficient of thermal conductivity in associated compounds. The level of association diminishes rapidly as the molecular weight increases, since it is easier for the particles of larger mass to break the hydrogen bond in the case of thermal fluctuations, and the smaller the associates, the lower the thermal conductivity.

With increasing temperature the destruction of complexes occurs more rapidly in the case of  $D_2O$  than in the case of  $H_2O$  [25]. This apparently causes the thermal conductivity of the  $D_2O$  to be smaller than that of the  $H_2O$  and for the displacement of the thermal-conductivity maximum at identical  $D_2O$  isobars to be smaller than in the case of  $H_2O$ .

Having examined the  $H_2O$  thermal-conductivity isobars from [18] and the  $D_2O$  isobars of this paper, we can see that with an increase in temperature the thermal conductivity reaches a certain point, subsequent to which it diminishes. The following process is taking place here: first of all, we have an elevation in the intensity of the molecular thermal motion, i.e., thermal conductivity; secondly, the number of molecules per unit volume diminishes, i.e., heat carriers; third, the number of associates is reduced, and the smaller this number, the lower the magnitude of the thermal conductivity. The combined effect of these factors governs the magnitude of the thermal conductivity.

Figure 1b shows a plot of the  $D_2O$  coefficient of thermal conductivity versus density, while Fig. 2 shows the relationship between the  $H_2O/D_2O$  ratio of the thermal conductivities and temperature at various pressures.

We have derived a relationship to describe the experimental data of the  $D_2O$  coefficient of thermal conductivity to temperatures up to 200 $^{\circ}C$ , and this relationship has the form

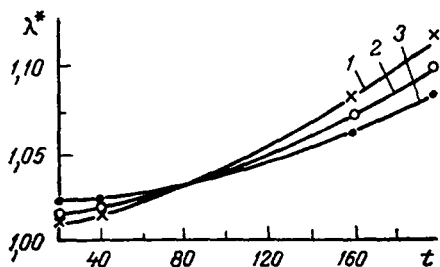


Fig. 2. Relationship of  $\lambda^* = \lambda_{H_2O} / \lambda_{D_2O}$  to temperature at various pressures: 1)  $P = 400$  MPa; 2) 200; 3) 20.  $t$ , °C.

TABLE 1. Thermal Conductivity  $\lambda$  of Heavy Water, mW/(m·K)

P, mPa	Temperature, °C									
	20	40	60	80	100	120	140	160	180	200
0,1	591	611	626	635	—	—	—	—	—	—
20	600	621	636	647	653	653	649	642	629	613
40	610	631	646	657	664	664	662	656	644	630
60	621	643	657	668	675	675	675	670	657	646
80	629	650	666	678	686	685	685	683	674	664
100	638	660	676	688	698	698	698	694	686	675
120	644	667	683	696	707	710	712	707	700	691
140	651	675	691	703	715	720	723	718	712	703
160	658	683	699	713	724	729	735	730	726	718
180	666	690	707	720	733	739	743	742	736	729
200	675	699	717	729	742	750	754	752	747	739
220	682	706	724	739	752	759	765	763	758	750
240	690	713	730	745	760	769	773	772	768	760
260	698	721	739	751	765	775	777	780	777	772
280	704	728	745	758	772	783	785	786	785	781
300	710	735	751	765	779	791	792	794	791	790
320	716	741	758	773	788	796	800	803	802	799
340	722	747	765	779	793	801	809	813	811	809
360	729	753	772	786	800	807	818	820	820	817
380	737	760	778	793	807	815	823	826	826	825
400	743	766	784	801	815	822	829	833	833	832

$$\lambda_{(P,t)} = \lambda_{s(t)} \left( 1.990 \frac{\rho_{(P,t)}}{\rho_{s(t)}} - 0.990 \right).$$

In this relationship the values of the D<sub>2</sub>O thermal-conductivity coefficient at the saturation line have been taken from [16], the D<sub>2</sub>O densities at the saturation line have been taken from [15], and the densities below 100 MPa are obtained from [15, 26], below 350 MPa from [27], and below 400 MPa at a temperature of 25°C, these data are from [28], and the remaining density data have been derived by calculation. The relationship describes the experimental D<sub>2</sub>O data for pressures up to 400 MPa and below temperatures of 200°C with an error of 1.3% (see Table 1).

#### NOTATION

$\lambda$ , the thermal conductivity;  $\lambda_s$ , the thermal conductivity of the D<sub>2</sub>O at the saturation line;  $\rho$ , the density of the D<sub>2</sub>O;  $\rho_s$ , the density of the D<sub>2</sub>O at the saturation line; P, pressure; t, temperature.

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